

## UNIVERSITI TEKNIKAL MALAYSIA MELAKA

# THE INVESTIGATION ON THE FATIGUE CRACK GROWTH ON WELDED PRESSURE VESSEL STEEL

This report is submitted accordance with requirement of Universiti Teknikal Malaysia Melaka (UTeM) for Bachelor Degree of Manufacturing Engineering (Engineering Material) with Honours.

by

## MOHD KHAIRUL ADLI BIN MOHD ZIN

# FACULTY OF MANUFACTURING ENGINEERING 2009

	KNIKAL MALAYSIA MELAKA
BORA	NG PENGESAHAN STATUS LAPORAN PSM
	JUDUL:
The Investigation of The	Fatigue Crack Growth On Welded Pressure Vessel Steel
	SESI PENGAJIAN:
	Semester 2 2008/2009
Saya Mohd Khairul Adli Bin	Mohd Zin
•	an PSM / tesis (Sarjana/Doktor Falsafah) ini disimpan di ikal Malaysia Melaka (UTeM) dengan syarat-syarat kegunaan
2. Perpustakaan Universiti Te	h hak milik Universiti Teknikal Malaysia Melaka dan penulis. eknikal Malaysia Melaka dibenarkan membuat salinan untuk Jongan izin penulis
SULIT	(Mengandungi maklumat yang berdarjah keselamatan atau kepentingan Malaysia yang termaktub di dalam AKTA RAHSIA RASMI 1972)
TERHAD	(Mengandungi maklumat TERHAD yang telah ditentukan oleh organisasi/badan di mana penyelidikan dijalankan)
√ TIDAK TERHAD	
	(TANDATANGAN PENYELIA)
(TANDATANGAN PENULIS)	
Alamat Tetap:	Cop Rasmi:
No. 16, Kg. Tengah 1,	3 C Universiti Teknikal Malaysia Melaka

\* Jika laporan PSM ini SULIT atau TERHAD, sila lampirkan surat daripada pihak organisasi berkenaan dengan menyatakan sekali sebab dan tempoh tesis ini perlu dikelaskan sebagai SULIT atau TERHAD.

## DECLARATION

I hereby, declared this thesis entitled "The Investigation on the Fatigue Crack Growth on Welded Pressure Vessel Steel" is the results of my own research except as cited in references.

Signature	:	
		Mohd Khairul Adli Bin Mohd Zin
Author's Name	:	
		6 April 2009
Date	:	

## APPROVAL

This report is submitted to the Faculty of Manufacturing Engineering of UTeM as partial fulfillment of the requirements for the degree of Bachelor of Manufacturing Engineering (Engineering Materials) with Honours. The members of the supervisory committee are as follow:

(Signature of Supervisor)

-----

En. Mohamad Haidir Bin Maslan

(Official Stamp of Supervisor)

## ABSTRACT

This project (Projek Sarjana Muda) studied the fatigue crack growth (FCG) of commonly industry used welded pressure vessel steel. In the oil and gas industries, the welded pressure vessel steel was affected by the welding heat output that causes many changes to the mechanical and metallurgical properties on near as-welded region (HAZ) effecting fatigue crack growth (FCG) rate on its interface. This leads to many accidents involving failure of pressure vessels. The objective of this project is to investigate and study about the fatigue crack growth (FCG) on the base metal (BM) region, and heat affected zone (HAZ) region of the welded pressure vessel steel. The type of tested steel is ASTM 516 Grade 70 of thickness 12mm. The steel was welded using submerged arc welding, and undergone post weld heat treatment. Then, it is fabricated to compact tension C(T)specimen according to ASTM E647-03. Two different notch location of compact tension specimens were fabricated relatively according to the heat affected region, and base metal region. The microstructure analysis was done and resulted ferrite-pearlite in BM region, and ferrite, austenite and cementite in the HAZ, while the WM has ferrite, widmanstatten ferrite and bainite. The hardness test was also done using Rockwell Hardness testing and found HAZ region had the highest value than BM region. These two specimens were fatigue cyclic loaded according ASTM E 647-03 and found that the HAZ region had the highest FCG rate compared to the BM FCG rate because of the brittle structures of the HAZ regions. Finally, the ruptured surface of the specimens was done fractograph analysis under scanning electron microscope (SEM) and found that modes of fracture formations involved in both HAZ and BM regions are the same and slightly differences that are transgranularmixed and equiaxed dimples, quasi and mixed modes fracture, and fine cleavage and transition from large to small dimples of fracture on pre-crack, FCG and rupture regions respectively.

## ABSTRAK

Projek Sarjana Muda ini mengkaji pemanjangan keretakan kelesuan pada besi yang digunakan untuk besi tangki bertekanan di industri. Didalam industri minyak dan gas, kesan haba dari kimpalan menyebabkan perubahan sifat mekanikal dan metallurgi kepada kesan haba kimpalan yang memberikan kesan kepada pemanjangan keretakan kelesuan yang membawa kepada banyak letupan berlaku. Objektif projek ini untuk mengkaji pemanjangan keretakan kelesuan pada bahagian kesan haba kimpalan dan besi utama besi tangki bertekanan yang telah dikimpalkan. Jenis besi yang diuji adalah ASTM A516 gred 70 berketebalannya 12 milimeter. Kepingan besi dipateri menggunakan ark kimpalan automatik dan menjalani proses rawatan haba. Kemudian, besi tadi di fabrikasi mengikut bentuk mampat-tegangan spesimen mengikut panduan ASTM E647-03. Dua bentuk mampat-tegangan spesimen dibentuk mengikut kedudukan bahagian kesan haba kimpalan dan besi utama. Analisis mikrostuktur dilakukan dan mendapati mikrostruktur "ferritepearlite" in besi utama (BM), "ferrite, austenite dan cementite" di kawasan kesan haba kimpalan, dan besi kimpalan, (WM) ada "ferrite, widmanstatten ferrite dan bainite". Ujian kekerasan dilakukan melalui Mesin Ujian Kekerasan Rockwell mendapati nilai kekerasan kesan haba kimpalan tinggi berbanding besi utama. Kedua spesimen dijalankan ujian pemanjangan keretakan kelesuan mengikut "Pengukuran Kadar Pemelajaran Kelesuan Keretakan" (ASTM E647-03) mendapati kesan haba kimpalan (HAZ) mempunyai kadar pemelajaran keretakan tinggi berbanding besi utama (BM) disebabkan rapuhnya kesan haba kimpalan (HAZ). Selepas itu, spesimen yang sepenuhnya retak dijalankan analisis fractograf dibawah mesin Misroskop Imbasan Elektron mendapati mod keretakan sama dan tidak banyak berbeza di dalam kesan haba kimpalan dan besi utama iaitu campuran antaragranular, campuran mod keretakan, perubahan unjuran besar ke kecil pada pra-retak, kelesuan keretakan, dan kawasan gagal masing-masing.

## DEDICATION

To my beloved parents and grandmother Hajah Normah Bte Sulaiman Mohd Zin Bin Mohd Amin Hajah Halijah Bte Md. Don

### ACKNOWLEDGEMENT

I would to expresses my gratitude to Allah, the most gracious and most merciful for giving me guidance in accomplishing this research project. The highest of appreciation to research project (*Projek Sarjana Muda*) supervisor, *Encik Mohamad Haidir Bin Maslan* in giving me guidance throughout the project flow and understanding throughout this the project. Repeated uncorrected tasks, format, and involving this project have been corrected by his guidance prior to this project title. This appreciation also goes to the examiner, *Dr. Jariah bt. Mohamad Juoi* that will be evaluating this project report and presentation along with the supervisor. Not to forget *Miss Liew Pay Jun* that evaluated my presentation skills during the project presentation. In this text also, the appreciation to the lecturers, and technicians in involved helping and provide me guidance to throughout this project. And lastly, credits to my parents and family that gives their morale support in completing this project and my everyday life generally.

## **TABLE OF CONTENTS**

Decla	Declaration i				
Appro	Approval				
Abstr	Abstract				
Abstr	ak	iv			
Dedic	eation	v			
Ackn	owledgement	vi			
Table	e of Contents	vii			
List o	of Tables	х			
List o	of Figures	xi			
List o	f Abbreviations, Symbols and Nomenclature	XV			
1. CH	IAPTER 1: INTRODUCTION	1			
1.1	Introduction	1			
1.2	Background	1			
1.3	Problems statement	2			
1.4	Research objectives	3			
1.5	Scope of the project	4			
1.6	Design of project	5			
2. CH	IAPTER 2: LITERATURE REVIEW				
2.1	Pressure vessel steel	6			
2.2	Submerged arc welding	8			
2.2.1	Post weld heat treatment principles	9			
2.2.1.	1 Post weld heat treatment	10			
2.2.1.	2 Thermal stress relief	10			
2.2.2	Weld stresses	11			
2.3	Fracture mechanics	15			
2.3.1	Ranges of applicability of fracture mechanics	16			
2.3.1.1 Linear elastic fracture mechanics (LEFM) 16					

2.3.1.2	Elastic plastic fracture mechanics (EPFM)	22
2.3.2	Fracture mechanics testing	25
2.3.3	Fatigue crack growth	29
2.3.4	Literature review on the fatigue crack growth	31
2.3.4.1	Crack in single a phase microstructure interface	31
2.3.4.2	Crack in dual phase microstructure interface	32
2.4	Weldment microstructures and properties	34

#### **3. CHAPTER 3: RESEARCH METHODOLOGY**

3.1	Introduction to research methodology 40			
3.2	Research design 41			
3.3	Material 4			
3.3.1	Glow Spark Spectrometry composition data	42		
3.4	Equipment and usage	42		
3.5	Sample Preparations	44		
3.5.1	Welding	45		
3.5.2	Post weld heat treatment	46		
3.5.3	Glow discharge spectrometry	47		
3.5.4	Fabrication	49		
3.6	Experiment	51		
3.6.1	Microstructure analysis (ASTM E340)	51		
3.6.2	Tensile Test (ASTM E8M)	52		
3.6.3	Hardness test 5			
3.6.3.	1Rockwell (ASTM E18)	54		
3.6.4	The fatigue crack growth test (ASTM E647)5			
3.6.4.	1 The fatigue pre-cracking test	56		
3.6.4.2	2 The fatigue crack growth test (FCG)	58		
3.6.4	Fractograph analysis	58		
4. CH	APTER 4: RESULT AND DISCUSSION	59		
4.1	Introduction	59		

4.2 Microstructure analysis (ASTM E340) 59

4.3	Tensile test evaluation	61	
4.5	Hardness test evaluation 6		
4.6	The fatigue crack growth result analysis (ASTM E367).	64	
4.6.1	The fatigue crack growth analysis of both BM and HAZ	65	
4.7	Fractograph analysis result	66	
5.0	CHAPTER 5: CONCLUSION AND RECOMENDATIONS	69	
5.1	Conclusion	69	
5.2	Suggestion for future work	70	
REF	ERENCES	72	
APP	ENDICES	77	
A	Gantt chart of PSM	77	
В	Engineering drawing of the Compact Tension Specimen, C(T)	81	

## LIST OF TABLES

2.1	The ASTM designation for pressure vessel carbon steel	7
3.1	The material of the sample	
		4
	2	
3.2	The actual compositions contained in the welded ASTM 516 Grade 70 steel.	
	42	
3.3	The equipments involve in the project	
	43	
3.4	The data applied in fatigue precracking test	
	57	
3.5	The data applied in fatigue crack growth test	
	58	
3.6	The magnification data on each region	
	58	
4.1	The comparison of actual data and the supplier of material	

## **LIST OF FIGURES**

2.1	Schematic diagram of submerged arc welding	
	8	
2.2	The submerged arc welding widely used in fabrication of pressure vessel	
	9	
2.3	Longitudinal (L) and transverse (T) Shrinkage Stress in a Butt Join Weld	12
2.4	Schematic representation of distortion in a butt joint	12
2.5	The Typical Distribution of Longitudinal ( $\sigma_{\chi}$ ) and Transverse Residual	
	Stress( $\sigma_y$ ) in a Butt Joint along the weld line (X-Axis) and the line vertical	
	to the weld line passing through the center of the weld (Y-axis)	14
2.6	Mode 1; Tension and opening	16
2.7	The Irwin plastic zone	18
2.8	Schematic representation of y component of normal stress $\sigma_y$ along line directly crack tip ( $\theta = 0$ )	of 19
2.9	Dugdale strip yield model	20
2.10	Variation in fracture toughness with plate thickness	21
2.11	The various stress-strain curves	22
2.12	The hinge model for estimating CTOD from three-point bend specimens	24
2.13	The comparison of the stress-strain behavior of elastic-plastic and nonlinear elas	tic
	materials	24
2.14	Fracture mechanics testing (SENB)	26
2.15	Examples of common fracture toughness test specimen types	27
2.16	The various a versus N curves can be generated by varying the magnitude of the	
	cyclic loading and/or the size of the initial crack	30
2.17	The fatigue crack growth data is a log-log plot of da/dN versus $DK_{l}$ .	30
2.18	A schematic diagram showing the interaction between the heat source and the	
	base metal	34
2.19	Allotriomorphic & idiomorphic ferrite.	36
2.20	Morphology of primary and secondary Widmanstatten ferrite	
	37	
2.21	The deformations boundary types	
	37	

3.1 The flow chart of the research design in this project

3.2	Figure shows the schematic illustration of the Instron FastTrack ™ 8800	
	Series	22
3.3	The flow chart of sample preparation	45
3.4	The illustrations of the welding combinations of steel plates	45
3.5	The illustrations of base material are weld together on one side opposing	
	each other. (b) The yielded welded surface	46
3.6	Flow chart of the post weld heat treatment	46
3.7	Schematic of a glow discharge spectrometer source	48
3.8	The Sample of weld material	48
3.9	The several of notch position on the sample	49
3.10	The isometric view of the standard compact-tension C (T) specimen for	
	fatigue crack growth rate testing	50
3.11	The standard compact-tension C (T) specimen for fatigue crack growth	
	rate testing	50
3.12	The dimension of the tensile specimen of the base metal plate	53
3.13	The point of indentation on grid size on the welded steel	54
3.14	The etching process	55
3.15	The surface yield of the etchant	55
3.16	Figure illustrates the dynamic loading exerted on the sample	57
4.1	Figure shows the BM microstructure with bands of (a) preutectoid ferrite (whit	te)
	and (b) pearlite (dark). (Magnification 200X)	60
4.2	Figure shows the HAZ microstructure with acicular ferrite surrounded by prior	
	austenite grain boundary and cementite network. (Magnification 200X)	60
4.3	Figure shows the WM microstructure showing grain boundary of ferrite, side-p	late
	ferrite, Widmanstätten ferrite, and bainite. (Magnification 200X)	60
4.4	The ruptured base metal of tensile test	61
4.5	Figure shows the graph of the Strain (N/mm <sup>2</sup> ) versus Stroke Strain (%)	60
4.6	Figure show the (a) welded steel sample and its (b) hardness distribution on we	elded
	steel sample.	60

4.7	Graph shows the total crack length versus the cyclic loading exerted to the BM a	ind
	HAZ.	64
4.8	Graph shows the da/dN versus stress intensity factor, dK for both of BM and HA	Z.
		64
4.9	The overview of the rupture base metal specimen (a) top view, and (b) side view	ι.
		67
4.10	Figure shows the transgranular and mixed fatigue-fracture surface of the preci	rack
	region of the BM steel plate.	67
4.11	Figure show the quasi-cleavage fracture was found on the crack growth fract	ture
surface	e of BM steel plate	68
4.12	Figure shows the fine cleavage fracture rupture surface of BM steel plate	68
4.13	Fractograph showing equiaxed dimples in the HAZ fractured surface at the preci	rack
	region	69
4.14	Fractoraph showing mixed mode fracture with facet and dimples in the HAZ on	the
	crack growth fracture surface.	69
4.15	Fractograph showing transition from a mixed mode large dimpled fracture t	to a
small d	limpled ductile fracture at the ruptured surface of the HAZ	70

## LIST OF ABBREVIATIONS, SYMBOLS & NOMENCLATURE

LPG	-	Liquefied petroleum gas
Psig	-	pound-force per square inch gauge
ASTM	-	American Society for Testing and Materials
WM	-	Weld metal
HAZ	-	Heat affected zone
BM	-	Base metal
MPa	-	Mega Pascal
SAW	-	Submerged arc welding
DC	-	Direct current
AC	-	Alternating current
SS	-	Stainless steel
$\sigma_x$	-	Longitudinal stress
$\sigma_y$	-	Transverse stress
$\sigma_m$	-	Maximum stress
f	-	Residual stress
LEFM -	Linear e	elastic fracture mechanics
EPFM	-	Elastic-plastic fracture mechanics
K <sub>1</sub>	-	Stress intensity factor
G	-	Energy release rate
γ <sub>s</sub>	-	Specific surface energy

$\gamma_p$	-	Plastic deformation energy
α	-	Applied stress
а	-	Crack length
E	-	Modulus of elasticity
a*	-	Effective crack length
r <sub>p</sub>	-	Circular plastic zone of radius
θ	-	Angular coordinate
t <sub>xy</sub>	-	Torque stress
$\sigma_{xy}$	-	Elastic-plastic boundary
r	-	Radius
r <sub>y</sub>	-	Plain stress and plain strain
K <sub>eff</sub>	-	Effective stress intensity factor
С	-	Internal crack length
t	-	Thickness
K <sub>IC</sub>	-	Fracture toughness
K <sub>C</sub>	-	Maximum fracture toughness
CTOD	-	Crack-tip opening displacement
d	-	Crack-tip opening displacement (changes)
$d_{el}$	-	Crack-tip opening displacement (elastic)
$d_p$	-	Crack-tip opening displacement (plastic)
SENB	-	Single edge notch bend
ESIS	-	The European Structural Integrity Society
ССТ	-	Centre-cracked tension (CCT)
SENT	-	Single edge notch tension
da/dN	-	Crack growth rate per cycle of loading
DK	-	Stress-intensity factor at the tip of the crack
FCG	-	Fatigue crack growth
JLF-1	-	Reduced activation steel type
Cr	-	Chromium
AISI	-	American iron and steel institute
00	-	Alpha designation ferritic grains
CGB	-	Coarse-grained bainitic
FGB	-	Fine-grained bainitic
ICR	-	Inter-critical region

CGHAZ-Coarse-grained heat affected zone

FGHAZ- Fine-grained heat affected zone

- PWHT Post weld heat treatment
- FCAW-S- Self shielded flux-cored arc-welding
- Al Aluminium
- Ti Titanium
- Zr Zirconium
- EDM Electric discharge machining
- GDS Glow Discharge Spectrometry

# CHAPTER ONE INTRODUCTION

#### 1.1 Introduction

In the revolution of oil and gas in our industrial world, it involves the applications of pressure vessel. Pressure vessels is used to hold gases or liquids at a pressure different from the ambient pressure or designed as a closed container. For fundamental uses, pressure vessel is used as a vessel, tanks, and pipelines that carry, store, or receive fluids. In the industry world, pressure vessels are used in a variety of applications such as industrial compressed air receivers and domestic hot water storage tanks. Other examples of pressure vessels are diving cylinder, recompression chamber, distillation towers, autoclaves and many other vessels in mining or oil refineries and petrochemical plants, nuclear reactor vessel, habitat of a space ship, habitat of a submarine, pneumatic reservoir, hydraulic reservoir under pressure, rail vehicle airbrake reservoir, road vehicle airbrake reservoir and storage vessels for liquefied gases such as ammonia, chlorine, propane, butane and Liquefied petroleum gas (LPG).

#### 1.2 Background

Pressure vessels are built with good tensile properties that is chemically stable in the chosen application can be employed. The mechanical properties of steel are increased by forging, but welding can sometimes reduce these desirable properties. In case of welding, in order to make the pressure vessel meet international safety standards, carefully selected steel with a high impact resistance & corrosion resistant

material should also be used. Some pressure vessels are made of wound carbon fibre held in place with a polymer. Due to the very high tensile strength of carbon fibre these vessels can be very light, but are much trickier to manufacture.

However, there are many accidents involving pressure vessel steel and boilers. And it had become a common problem in the uses of these pressure vessels. For example, the accident on July, 2002, an Enbridge 34-inch-diameter-steel pipeline ruptured in a marsh west of Cohasset, Minnesota, America. Approximately 6,000 barrels (252,000 gallons) of crude oil were released from the pipeline as a result of the rupture. No deaths or injuries resulted from the release. The cost of the accident was approximately \$5.6 million, which includes the cost of cleanup and recovery, value of lost product, and damage to the property of the pipeline operator and others. The National Transportation Safety Board determines that the probable cause of the July 4, 2002, pipeline rupture near Cohasset, Minnesota, was inadequate loading of the pipe for transportation that allowed a fatigue crack to initiate along the seam of the longitudinal weld during transit. After the pipe was installed, Cavaney (2004) found that fatigue crack grew with pressure cycle stresses until the crack reached a critical size and the pipe ruptured.

Another example, January 20, 2004, after an explosion at Algeria's largest refinery and principal oil exporter in the port city of Skikda. Rescue workers searched through rubble for missing worker on Tuesday after a huge explosion at its key gas installations killed 23 people on Monday evening, official media said. It caused by a defective, high pressure, steam boiler ruptured, high vibrations just before the boiler ruptured. The resultant explosion on rupture damaged nearby vessels containing flammables. The flammable Loss of Containment resulted in further fires and explosions. (Anonymous, 2004)

#### **1.3 Problem statement**

This behaviour crack growth has become an undesired phenomenon that occurs to the pressure vessel steel. Pressure vessel steel was widely been used in pipings, storage tanks or container that is that operated at pressures above 15 *psig* or etc. This presence of crack can cause many safety hazards. This cyclic fatigue growth is a phenomenon in structures subject to cyclic actions involving progressive localized damage, with cracks and crack propagation. Crack may initiate originally undamaged areas and propagate afterwards, and already existing cracks and crack-like defects propagate. The process eventually leads to a reduction of cross-sectional areas to such an extent that rupture occurs under an action of a magnitude that has been withstood satisfactory before. Zeman *et al.* (2006) stated that final structure will be ductile or brittle.

Recently, safety organizations have discovered during inspections that there are a number of welded pressure vessels that are cracked and damaged in workplaces. When pressure vessels have cracks or damage, they become unsafe. The cracks or damage may result in leakage or rupture failures. Failure, when dealing with pressure vessels and such high *psig*, can present major safety issues. The commonly used pressure vessel steel type is ASTM SA516 Grade 70 steel, the interested argument in this research is;

"How does the fatigue crack growth rate of the welded pressure vessel ASTM A516 Grade 70 of the heat affected zone and base metal regions?"

#### **1.4 Research objectives**

In this project, there are two main objectives that have to be achieved in order to fulfil the requirements of the project. These objectives are identified and analyzed from series of discussion and references made regarding the problem statement;

- To investigate the fatigue crack growth on welded pressure vessel steel in two different crack propagation regions that are the base metal (BM) region, and heat affected zone (HAZ) region.
- To compare the fatigue crack growth rate and behaviour on each region studied.

#### **1.5** Scope of the project

The joining process of welding two or more pressure vessel steels will affect or vary along with the properties of the pressure vessel steels. The welded pressure vessel steel is composed to several of heterogeneous microstructural regions composed to base metal (BM), heat affected zone (HAZ), and weld metal (WM). Variations in the properties may due to the high heat input during welding, slag inclusions, chemical reactions of the metal to the atmosphere of flux or filler material, disproportionate heating or cooling rates (Sindo *et al.*, 1987). These microstructural regions of its microstructure and properties are altered by welding heat from the welding process and subsequent re-cooling causes this change in the area surrounding the weld.

The extent and magnitude of property change depends primarily on the base metal (BM), the weld filler metal, and the amount and concentration of heat input by the welding process. The extent and magnitude of property change gradually from WM to HAZ to BM. The property changes include changes in chemical reactions, mechanical properties, microstructures, grain size, and etc. having each regions have different yield strength, tensile strength, and fracture toughness. The grains near the weld are coarser gradually changing finer towards the base metal. This change of property is most discussed at weld interface, which is the boundary separating the WM from the HAZ. Thus when crack develops in the weld metal or outside the weld metal in the heat affected zone and starts propagating, it encounters different set of properties as it advances. In particular, when it encounters the weld interface, its behaviour changes according to its orientation and point of initiation in weldment relative to the interface.

Thus, the scope of this project are to compare the fatigue crack propagation of welded ASTM 516 Grade 70 steel plate on different regions of base metal (BM) and heat affected zone (HAZ). The microstructure analysis is done to identify the micro structural surface of the welded ASTM 516 Grade 70 steel plate. The hardness test is conducted to analyze the hardness distribution of the welded ASTM 516 Grade 70 steel plate. Also the tensile test is done to obtain the yield point, and the tensile strength. And lastly, the fractograph analysis is done to analyze its ruptured surface.

#### **1.6 Design of the project**

The aim of this work is the analysis of fatigue crack propagation in the sample material on two different regions of base metal, and heat affected zone of the ASTM 516 Grade 70 steel plate. These tests were done in compact tension specimen according to the ASTM E647 standard test procedure. The cyclic loading was done by the Instron Cyclic Fatigue Loading Machine. Finally, fracture surfaces morphology (fractograph analysis) was conducted by scanning electron microscope (SEM) on each of sample regions after completely plasticity failure in regions of the pre-crack, fatigue crack growth, and rupture regions respectively.

# CHAPTER TWO LITERATURE REVIEW

#### 2.1 Pressure vessel steel

Chattopadhyay (2005) defines pressure vessel as a closed container with a pressure differential between inside and outside. Pressure vessel like vessels, tanks, and pipelines that used to carry, store, or receive fluids. Pressure vessels often have a combination of high pressures together with high temperatures and in some cases flammable fluids of highly radioactive materials. Because of such hazards it is imperative that the design be such no leakage can occur. In addition, these vessels have to be designed carefully to cope with the operating pressure and pressure. The rupture of a pressure vessel has a potential to cause extensive physical injury and property damage.

The pressure vessels steels usually are fabricated from carbon and alloys. The standard specifications for general requirements according to the American Society for Testing and Materials (ASTM) for steels plates for pressure vessels of carbon types are listed in the in the Table 2.1.