VIBRATION ANALYSIS OF A PLATE WITH THREE PARALLEL HORIZONTAL CRACKS

TIEW YONG LEEK B141710074

BMCG

alwin1234561@gmail.com



Faculty of Mechanical Engineering Universiti Teknikal Malaysia Melaka June 2021

SUPERVISOR'S DECLARATION

I have checked this report and the report can now be submitted to JK-PSM to be delivered back to supervisor and to the second examiner.

UNIVSignature TEKNIKAL MALAYSIA MELAKA

Name of Supervisor :Date

APPROVAL

I hereby declare that I have read this project report and in my opinion this report is sufficient in terms of scope and quality for the award of the degree of Bachelor of Mechanical Engineering.



Abstract

In this report, the equation of motion of vibration analysis of a thin isotropic plate with three parallel horizontal cracks for a given set of boundary conditions is developed. Kirchoff's classical plate theory is applying to obtain the principles equilibrium and equation motion of an isotropic plate. Crack formulation on the plate is then presented from the application of Line Spring Model (LSM). After, Galerkin's method is used to find the solution of governing equation by applying weighted residual technique and convert the transverse function into time dependent function. The governing equation is then finalized by applying equation of three boundary conditions. Next, the Berger's formulation is applied to transverse the deflection terms of in-plane forces into a non-linear ordinary equation. The natural frequency of the plate is then become a variable by parameters of half crack length, length of plate, boundary conditions and number of cracks (single and multiple). The mathematical model result is presented in term of natural frequency are totally affect by half crack length and number of cracks and the result is validated by comparison with finite element analysis result.

UNIVERSITI TEKNIKAL MALAYSIA MELAKA

ABSTRAK

Dalam report ini, persamaan analisis gerakan getaran plat isotropik nipis dengan tiga retakan mendatar selari untuk satu set syarat sempadan telah dikembangkan. Teori plat klasik Kirchoff diterapkan untuk mendapatkan keseimbangan prinsip dan gerakan persamaan plat isotropik. Formulasi retakan pada plat kemudian disajikan dari aplikasi Line Spring Model (LSM). Setelah itu, kaedah Galerkin digunakan untuk mencari jalan penyelesaian persamaan dengan menerapkan teknik baki bobot dan mengubah fungsi melintang menjadi fungsi bergantung pada waktu. Persamaan yang mengatur kemudiannya diselesaikan dengan menerapkan persamaan tiga syarat sempadan. Seterusnya, rumusan Berger digunakan untuk meleraikan istilah pesongan daya dalam satah menjadi persamaan tidak linear. Kekerapan semula jadi plat kemudian menjadi pemboleh ubah mengikut parameter panjang retak separuh, panjang plat, keadaan sempadan dan bilangan retakan (tunggal dan berganda). Hasil model matematik yang dikemukakan dari segi frekuensi semula jadi benar-benar dipengaruhi oleh panjang retak separuh dan jumlah retakan dan hasilnya disahkan dengan perbandingan dengan hasil analisis elemen hingga.

اونيۈم سيتى تيكنيكل مليسيا UNIVERSITI TEKNIKAL MALAYSIA MELAKA

ACKNOWLEDGEMENT

Firstly, I wish to express my sincere gratitude and appreciation to Universiti Teknikal Malaysia Melaka for giving me the opportunity to gain personnel intelligent through this final year project. From the first semester of final year project till now, I am constantly learning and able to apply my academic knowledge related to Mechanical Engineering.

My final year project tittle is related to industry and maintenance engineering analysis especially in aircraft manufacturing. This project is serving as a platform for me to actively expand my Mechanical Engineer knowledge to a new and advance of mu current education. With this, I able to apply my Mechanical Engineer knowledge of what I have studied throughout the duration of my Mechanical Engineering course at UTeM. In addition of that, new knowledge was gained by referring and reading the past or recent articles which bring a lot of help to begin and finish my final year project. By these article support with my knowledge, I was finalized able to conduct a new equation to analyze my project with the tittle is Vibration Analysis of a Plate with three horizontal parallel cracks.

Next, I would like to express my sincere gratitude and appreciation to my academic supervisor, Dr Rainah binti Ismail. A fully guidance and help from Dr Rainah make my project was get on a smoothly schedule and make me clearly when I was beginning my project at semester 1. Besides, she also accepts my opinion and fully help on the problem that I meet during both semesters.

Finally, I wish to express my deep appreciation and gratefulness to my parents for tirelessly supporting me and guiding me on the right path. They always motivate me to achieve the best in whatever I undertake and lend a listening ear as well as provide words of wisdom and encouragement whenever I run into problems, stressful and difficulties throughout my project period.

CONTENT

CHAPTER	CONTENT	PAGE
	SUPERVISOR'S DECLARATION	ii
	APPROVAL	iii
	ABSTRACT	iv
	TABLE OF CONTENT	vii
	LIST OF FIGURES	Х
	LIST OF TABLES	xiii
	LIST OF ABBREVIATIONS	xvi
	LIST OF SYMBOLS	xvii
CHAPTER 1	INTRODUCTION	1
	1.1 Background	
	1.2 Problem Statement	3
	1.3 Objective	4 اويىۋىرسىيۇ
	1.4 Scope of Project UNIVERSITI TEKNIKAL MALAYS	5
CHAPTER 2	LITERATURE REVIEW	6
	2.1 Plate theory	6
	2.2 Past research of plate	7
	2.2.1 Vibration of plate	7
	2.2.2 Numerical analysis on vibratio	n of 8
	plate with crack	
	2.2.3 Simulation and experimental an	nalysis of 12
	a plate with crack	

CHAPTER 3	METHODOLOGY	15
	INTRODUCTION	15
	3.1 Mathematical modelling	17
	3.1.1 Classical Plate Theory	17
	3.1.2 Crack Formulation of plate	25
	3.1.3 Galerkin's Methods	32
	3.1.4 Berger Formulation	35
	3.2 Finite element analysis	40
	3.2.1 Methods to simulate the cracked plate	40
CHAPTER 4	Result and Discussion	42
	Introduction	42
	4.1 Analytical analysis	43
	4.2 Finite element analysis (FEM)	49
	4.2.1 The first three mode shapes of the infact plate with three difference boundary conditions 4.2.2 The first three mode shapes of the cracked plate with three difference boundary conditions	60 60
	4.3 Comparison analysis between mathematical	63
	modelling and finite element analysis	
	4.4 Discussion	68
	4.4.1 Discussion on the first mode of natural	68
	frequency on the trends of the result with the affecting	
	on the multiple cracks on the plate with CCFF, SSSS	
	and CCSS boundary conditions	
	4.4.2 Discussion on the other characteristics of	78
	physical parameters which will affect the natural	
	frequency of the plates.	
	4.4.2.1 Young modulus and Thickness of	79
	the plate	
	4.4.2.2 Density of the plate	81

CHAPTER 5	5.1 CONCLUSION	82
	5.2 RECOMMENDATION	83
	REFERENCE	84
	APPENDICE	88



List of figures

- Figure 2-1 Examples of the boundary conditions
- Figure 2-2 Relationship between crack depth ratio and crack compliance coefficients
- Figure 2-3 SSSS condition of Plate with difference crack depth ratios of plate
- Figure 3-1 Flow chart of methodology
- Figure 3-2 A plate with three parallel cracks on its surface
- Figure 3-3 In-plane forces of a plate with three parallel cracks
- Figure 3-4 Two dimensional of plate with three parallel cracks
- Figure 3-5 Boundary condition with their edge mode
- Figure 4-1 Three parallel horizontal cracks on the surface of the plate
- Figure 4-2 The shape and geometry of the plate
- Figure 4-3 First three mode of intact plate with CCFF boundary condition with plate A
- Figure 4-4 First three mode of intact plate with CCSS boundary condition with plate A
- Figure 4-5 First three modes of intact plate with SSSS boundary condition with plate A

- Figure 4-6 First three modes of three horizontal cracks of a plate with CCFF boundary condition and 10mm half crack length with plate A
- Figure 4-7 First three modes of three horizontal cracks of a plate with CCSS boundary condition and 10mm half crack length with plate A
- Figure 4-8 First three modes of three horizontal cracks of a plate with SSSS boundary condition and 10mm half crack length with plate A
- Figure 4-9 First mode natural frequencies of a single and multiple cracks in each boundary condition against half crack length at plate A
- Figure 4-10 First mode natural frequencies of a single and multiple cracks in each boundary condition against half crack length at plate B
- Figure 4-11 First mode natural frequencies of a single and multiple cracks in each boundary condition against half crack length at plate C
- Figure 4-12 First mode natural frequencies with a 25mm crack of a plate with different number of cracks in each boundary condition in

Plate B JNIVERSITI TEKNIKAL MALAYSIA MELAKA

- Figure 4-13 First mode natural frequencies of a multiple cracks for three different set of boundary conditions (CCSS, CCFF and SSSS) against the half crack length at plate A, B and C
- Figure 4-14 The location of the crack against natural frequency of a single cracked plate A in each boundary condition
- Figure 4-15 The location of the crack against natural frequency of a single cracked plate B in each boundary condition
- Figure 4-16 The location of the crack against natural frequency of a single cracked plate C in each boundary condition

- Figure 4-17 Young modulus of the plate A with three cracks against first mode natural frequency with CCSS boundary condition
- Figure 4-18 Thickness of the plate with three cracks against first mode natural frequency
- Figure 4-19 Density of the plate with three cracks against first mode natural frequency



List of tables

Mathematical modelling of a plate result comparison with
Israr (2009)
Mathematical modelling of a plate result comparison with
Ismail (2012)
Mathematical modelling of a plate results with single and
multiple cracks
Result comparison with Israr (2008) with the rectangular
plate (Plate A) by applying CCFF boundary condition
Result comparison with Israr (2008) with the 25mm cracked
rectangular plate (Plate A) by applying CCFF boundary
condition.
Finite element analysis results of a plate A with CCFF
boundary condition (FEA)
Finite element analysis results of a plate B with CCFF
boundary condition (FEA)
Finite element analysis results of a plate C with CCFF
boundary condition (FEA)

Table 4.9	Finite element analysis results of a plate A with CCSS	
	boundary condition (FEA)	
Table 4.10	Finite element analysis results of a plate B with CCSS	
	boundary condition (FEA)	
Table 4.11	Finite element analysis results of a plate C with CCSS	
	boundary condition (FEA)	
Table 4.12	Finite element analysis results of a plate A with SSSS	
	boundary condition (FEA)	
Table 4.13	Finite element analysis results of a plate B with SSSS	
	boundary condition (FEA)	
Table 4.14	Finite element analysis results of a plate C with SSSS	
Kurk	boundary condition (FEA)	
Table 4.15	Comparison of first mode natural frequency of a cracked	
Tops .	plate between Mathematical and FEM solution with CCSS	
1	plate	
Table 4.16	Frequency difference and percentage error between	
UNIV	mathematical modelling and finite element analysis of a cracked plate with CCSS boundary condition	
Table 4.17	Comparison of first mode natural frequency of a cracked	
	plate between Mathematical and FEM solution with SSSS	
	plate	
Table 4.18	Frequency difference and percentage error between	
	mathematical modelling and finite element analysis of a	
	cracked plate with SSSS boundary condition	

- Table 4.19Comparison of first mode natural frequency of a crackedplate between Mathematical and FEM solution with CCFFplate
- Table 4.20Frequency difference and percentage error between
mathematical modelling and finite element analysis of a
cracked plate with CCFF boundary condition



List of abrevation

CCSS	Opposite edges simply supported.
CCFF	Adjacent edges clamped.
SSSS	Simply supported on all edges.
LSM	Line Spring Model
MMS	Multi-scale methods
DQM	اوبيوس سيني نيڪ.Differentiate quadratic method
SHM	Structural health monitoring
FEM	Finite Element

LIST OF SYMBOLS

Q	Force per unit length	
М	Bending moment per unit length	
$2a_x$	Crack length on each crack	
M	Bending moment per unit length due to crack	
q _z	Lateral force	
ρ	Density of plate	
D	Flexural rigidity	
v	Poisson ratio	
n	In-plane force per unit length	
\overline{n}	In-plane force per unit length due to crack	
σ	Bending stress	
h S	Thickness of plate	
$a_{tt}, a_{bb}, a_{tb}, a_{bt}$	Crack compliance coefficients	
$\overline{\sigma}_{mn}$	Normal tensile stress at crack location	
\bar{m}_{mn}	Bending moment at cack location	
w(x, y, t)	Time dependent transverse function	
X _i	Modal function in x direction of crack plate	
Y _j DN	Modal function in y direction of crack plate	
8	Strain	
E UNIV	VERSITI TEKNIK Young modulus IA MELAKA	
A _{ij}	Arbitrary amplitude	
$\Psi_{ij}(t)$	Time dependent modal coordinate	
l	Length of plate	
P _{ij}	Complex in-plane force function	
Ω_{ij}	Excitation frequency	

CHAPTER 1

INTRODUCTION

1.1 BACKGROUND

Safety is one of the most important for every auto-mobile, especially airplane. During the flight, the airplane is not allowable landing until the destination is reached, thus the appearing failure of any part of the airplane is very dangerous. "A short analysis may give a long-term safety journey for life". Consider many engineering components used in the aerospace industries. The component's design should be more investigate and analysis such as a vibrating structure under many random cycles of pressure.

Sandwich panels are a structure made by a light-weight core, and a flat surface layer bonded to each lateral. In this case, light weight is one of the main important matter on the sandwich panels. Its light-weight properties are function to minimize the overall weight of the aerospace's body in order built up a highly thrust force for the transport. The one of the main applications of sandwich panel is on aircraft and called as aircraft panels. The outermost layer of the aircraft panel of the structure is made from a aluminum plate which considers a light weight, thin and high durability which can perform well during the flight, take-off or landing. It performs a highly resistance on surface wear, pressure attack, or damage and having a better lifting during the flight.

Vibration is a mechanical phenomenon in which a structure of the component undergoes oscillations that occur about an equilibrium point. Generally, vibration will bring a lot of negative effect that occur on every component especially in the lightweight structure with a thin geometric plate. The issue of applying the lightweight structure as the material may lead to produce a high vibration on its body. Over time, the occurring of the high vibrational effects on the lightweight structure, especially on the wing panels, may have long-term as well as short-term damaging or cracks. These effects may cause the wings produce the difference output on both side of the aerospace wings such as unable to balance the body of the aerospace. Thus, the condition of the plate should be analyzed and compared the health of the plate in every maintenance schedule.

Cracks happen on the aircraft wing panels is very dangerous that may bring bad accident to us. From the latest news in the July 2019, many cracks on the aircraft wings were found on an Airbus A380 superjumbo jets. The aviation company was requested to have a full-body analysis and checking for 25 of the early production of Airbus A380 superjumbo jets to ensure the safety of their aircraft.

In this project, we concentrate and evaluate on the aircraft wing structures that had been constructed as an isotropic plate with the presence of the vibration behavior. The plate panels are generally under transverse pressure on the outermost layer of aircraft wings and are subjected to natural and shear forces occurred in the plate plane. The plate panels may not perform as planned if they contain even a small crack will result in a complete loss of balance and cause failure.

1.2 Problem Statement

The rapid advancement of technologies has changed the way of every industry operates, where the structures of the components become lighter and thinner to be designed. One of the examples is the isotropic thin plate on the aircraft wing panels. However, the trend for the structure of the plate may lead to unwanted instances of high vibration and caused the crack to occur on the plate. In this case, it is very important to detect any defects or failures that occur inside the plate or on the surface of plate at the early stage of development. Vibration health monitoring is one of the methods used to ERSITI TEKNIKAL MALAYSIA MELAKA detect the defects, it defined as damage detection and detect the degradation of mechanical integrity by using the vibration signal to generate the data. One of the examples is install the vibration sensor, this may give the benefit that engineer allowed to spend fewer time taking manual measurement and having more time focus on problems that could lead to downtime or equipment failure. From the previous analysis on the research, many of the researchers only focus on the single type of the crack problem such as the crack-oriented surface or crack depth on the fixed axis. In the phenomena every crack has their different behavior, it is impossible that there will be only a single crack that was happen on one time. The crack on the plate might occurring

in many minor cracks at the same time. In this project, we are going to enhance the crack formulation developed by Ismail (2012) and Joshi (2014) and analyze the crack of the plate with three parallel cracks on the plate surface.

1.3 Objectives:

The objective of this project are as follows:

- 1. To develop mathematical modelling of a plate with a three parallel cracks with horizontal to x-direction.
- 2. To study the influence of the parallel cracks on the vibration characteristics of the plate
- 3. To verify the developed model through comparison of the results with finite element method

UNIVERSITI TEKNIKAL MALAYSIA MELAKA

1.4 Scopes:

The scopes of this project are:

- An aircraft panel structure is model as an isotropic thin flat plate with a multiple cracks. The cracked plate is subjected to horizontal and parallel to each other with the chosen CCSS, SSSS and CCFF boundary conditions and the derivation of mathematical modelling is based on classical plate theory.
- Type of material used in this investigation is an aluminum alloy of 5083 grade with dimension of plate study is limited to three plates with plate A (0.5 x 1.0 m x 0.01 m), plate B (1.0m x 1.0m x 0.01m) and plate C (0.5m x 0.5m x 0.01m).
- Load acting on the surface of the plate, q is assumed to be the same as previously used, which is 10 N.
- 4. The crack is located at the center, one-third and two-third from the y-axis of the plate and at all are in the middle on the x-axis of the plate with having 0.01 m and 0.025 m half-crack lengths.

CHAPTER 2

Literature review

2.1 Plate theory

Plate theories are numerical representation of the fundamentals of flat plates in solid mechanics that take on beam theory. Plates are defined as a flat structural with a thin structure compared to its planar sizes. Basically, the usual thickness to width ratio was about $\frac{h}{w} \ll 0.1$ of a plate structure. The thin behavior of the plate was helpful which able to reduce the complete three-dimensional structurer mechanic issue to a two-dimensional problem by applying Line Spring Model. The purpose of the plate theory is to determine the deflection and stresses in a plate with a force was applied on it.

From the 19 century, Kirchoff-Love theory was the most famous used in engineering. It was a two-dimensional numerical model that was used to measure the stresses and deflection in an isotropic plate which obtained to forces and moments. Kirchoff (1888) was using an assumption to develop Kirchoff-Love theory by expanding the Euler-Bernuolli beam theory. In

Kirchoff's assumption, it was suggested that the mid-surface plane can reduce the threedimensional plates into two-dimensional plates.

For the following kinematics assumption are as below:

- straight lines normal to the mid-surface remain straight after deformation.
- straight lines normal to the mid-surface remain normal to the mid-surface after deformation.
- the thickness of the plate stays remain during a deformation.

Since the Kirchoff-love theory was minimized the numerical equation of plate. These assumptions had been widely used for plate analysis and had been further discuss on 19-21 century.

2.2 Past research regarding to plates.

2.2.1 Vibration of plate

Leissa (1969) was published a book "Vibration of plate". The fundamental equation of

plate theory had been discussed in term of elastic plate. The classical equation was form by using Laplacian operator, the relationship of bending and twisting moment with displacement. By obtain the general solution of classical equation, fourier series was assumed into a variable. Besides that, the classical equation had been applied into many forms of plate such as polar, elliptical and rectangular. After that Leissa (1969) was undergoing a series of study on the analysis the plate in polar, elliptical and rectangular form. Leissa (1969) was analysis along 21types of boundary condition which occur on the plate such as the simply supported boundary